Closing a biorefinery cycle of giant reed through the production of microporous and reusable activated carbon for CO₂ adsorption

Nicola Di Fidio, Domenico Licursi, Monica Puccini, Sandra Vitolo, Anna Maria Raspolli Galletti

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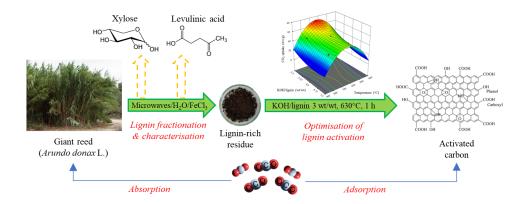
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1	Closing a biorefinery cycle of giant reed through the production of
2	microporous and reusable activated carbon for CO ₂ adsorption
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4	Nicola Di Fidio ^a *, Domenico Licursi ^a , Monica Puccini ^b , Sandra Vitolo ^b , Anna Maria Raspolli
5	Galletti ^a
6	
7	^a Department of Chemistry and Industrial Chemistry, University of Pisa, Via G. Moruzzi 13,
8	Pisa, Italy
9	^b Department of Civil and Industrial Engineering, University of Pisa, Largo Lucio Lazzarino,
10	Pisa, Italy
11	
12	*Corresponding author: Nicola Di Fidio
13	E-mail address: nicola.difidio@unipi.it
14	Telephone: +39 0502219210
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16	
17	ABSTRACT
18	The complete valorisation of all biomass components represents a crucial strategy for
19	developing new biorefinery schemes. This study completed a cascade biorefinery process
20	for the exploitation of holocellulose and lignin fractions of the non-food biomass giant reed
21	(Arundo donax L.). The residual lignin-rich solid fraction, obtained after the selective
22	conversion of hemicellulose and cellulose fractions to valuable bioproducts, was
23	characterised and activated by KOH treatment into microporous activated carbon (AC), to
24	be proposed for CO ₂ adsorption. The production of AC was optimised by the Design of

25 Experiments technique. Under the optimised process conditions (630 °C, KOH/lignin 3.0

wt/wt, 60 min) the AC yield was 34.4 wt% and the CO₂ uptake reached 72.3 mg/g, confirming the promising application of this biomaterial. Moreover, the obtained AC showed similar CO₂ uptake values over 10 cycles of adsorption/desorption tests, demonstrating its good recyclability, keeping its pristine CO₂ uptake capacity.

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Keywords: Biorefinery; Arundo donax L.; lignin-rich residue; activated carbon; CO₂
capture.

33

34 **1. Introduction**

The development of new biorefinery processes based on the complete exploitation of 35 renewable resources, such as lignocellulosic biomass, is crucial for achieving most of the 17 36 Sustainable Development Goals defined by the United Nations (United Nations, 2023). The 37 selective fractionation and conversion of the biomass components via chemical and/or 38 biological routes allow the synthesis of biofuels, green solvents, biomaterials, and fine 39 chemicals, to propose in substitution of fossil-based ones (Raspolli Galletti et al., 2021). A 40 sustainable solution to overcome the ethical contrast "food versus fuel" consists of the use of 41 42 waste or non-edible biomasses cultivated on marginal or polluted soils (Viccaro et al., 2022). Among non-edible crops, giant reed (Arundo donax L.) represents a suitable renewable 43 material for developing new biorefinery schemes, since it is a perennial grass characterised by 44 high production yield, even on marginal, contaminated, or underutilised lands, low water 45 demand, high polysaccharide content and good resistance to several pathogens (Pilu et al., 46 2014; Scordia and Cosentino, 2019). Traditional biorefinery processes generally produce a 47 lignin residue as the main side-stream, which is usually burned to produce energy with low 48 efficiency. However, lignin represents a renewable source of aromatic compounds (Di Fidio 49 et al., 2021b) or can be advantageously exploited through the production of new biomaterials, 50

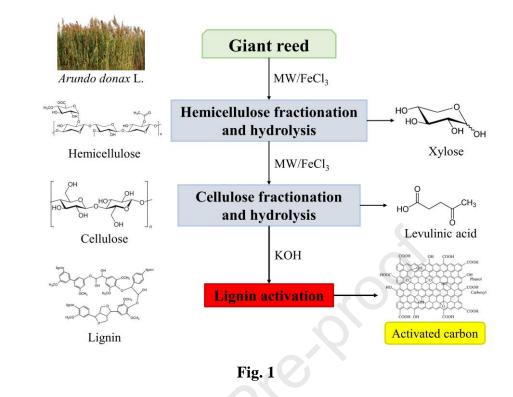
including activated carbon (AC) (Sellaoui *et al.*, 2023). ACs can be proposed for the adsorption of polluting gases, such as carbon dioxide, organic compounds (Allahkarami, Esmaeil *et al.*, 2023b; Nandi *et al.*, 2023; Xing *et al.*, 2023) and polluting cations/anions in aqueous solutions, such as Ni(II), Cu(II), nitrate, etc. (Allahkarami, Ebrahim *et al.*, 2022; Allahkarami, Ebrahim *et al.*, 2023). The most common biorefinery models of lignocellulosic biomasses are currently developed on the cellulose exploitation, paying much lower attention to the contemporary valorisation of hemicellulose and lignin fractions.

Bio-based microporous AC has attracted much interest in recent years since it represents a 58 sustainable and efficient adsorbent for the development of a plethora industrial applications. It 59 is a suitable alternative to traditional adsorbents, such as organic-inorganic hybrid sorbents, 60 zeolites, microporous polymers, and metal-organic frameworks, due to its several advantages, 61 such as low cost, high availability, high surface area, hydrophobicity, easy recyclability, and 62 low energy requirement for the regeneration of the pristine properties (Azmi et al., 2022; Guo 63 et al., 2023). In particular, the wastewater treatment (WWT) of municipal and industrial 64 effluents, and the adsorption of polluting gases represent two of the most studied AC 65 applications. ACs are used within WWT processes due to their high efficiency in adsorbing 66 several kinds of toxic pollutants, such as phenol and heavy metals (Allahkarami, Esmaeil et 67 al., 2023b; Rezai and Allahkarami, 2021). Remarkably, innovative ACs functionalised by 68 magnetic metals have been recently employed for phenol removal from aqueous solutions, by 69 this way improving the AC adsorption efficiency and its next recovery/reuse (Allahkarami, 70 Esmaeil et al., 2022, 2023a). 71

Unfortunately, pure lignin and lignin-rich residues are generally characterised by a very low surface area, due to their macroporous or non-porous structure, thus hampering their efficient employment for adsorption uses. For this reason, a physico-chemical activation step is necessary for obtaining a microporous and functionalised texture, which is a highly

desirable property for industrial applications (Alcañiz-Monge *et al.*, 2022; Heidarinejad *et al.*, 2020; Supanchaiyamat *et al.*, 2019). Chemical activation offers significant advantages with respect to the physical one, since the former allows the choice of different precursors and activating agents to produce ACs in high yields and with better tailored surface properties (Alcañiz-Monge *et al.*, 2022). Furthermore, CO_2 uptake is strictly related to the basicity of AC as well as to the activation conditions used for the biomass thermal processing (Malini *et al.*, 2023).

The present work deals with an innovative thermochemical valorisation of the lignin-rich 83 residue recovered at the end of a cascade process previously optimised by us for the raw 84 Arundo donax L. (Di Fidio et al., 2019; Di Fidio et al., 2020a). This carbon-rich biomaterial 85 was selected as the precursor for AC production, representing the final waste of the cascade 86 process developed for the tailored valorisation of polysaccharides, and its further valuable 87 exploitation was proposed in the perspective of the Circular Economy criteria. In this context, 88 the present biorefinery scheme aims at closing the circle of the complete and profitable 89 exploitation of the starting renewable material (Fig. 1). 90





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Figure 1 shows the schematic representation of the cascade biorefinery implemented to 95 obtain valuable polysaccharide derivatives and the lignin-rich residue, which was used in this 96 work as the precursor for the production of ACs suitable for CO₂ adsorption. A tailored 97 conversion of the holocellulose was optimised in our previous works. In the first step, the 98 conversion of hemicellulose catalysed by FeCl3 under microwave (MW) irradiation co-99 produced xylose and a solid residue enriched in cellulose. The latter was then used as the 100 feedstock for the subsequent conversion of glucan to levulinic acid and formic acid catalysed 101 again by FeCl₃ under MW irradiation, but working under harsher reaction conditions (Di 102 Fidio et al., 2019; Di Fidio et al., 2020a). This final lignin-rich residue represents the starting 103 feedstock to produce AC, by using KOH as the activating agent. The process conditions for 104 105 this activation treatment have been optimised by adopting the Design of Experiments (DoE) technique based on the Response Surface Modelling (RSM). The process implementation has 106 been devoted to obtaining ACs characterised by tailored surface properties, mainly in terms of 107 specific surface area and porosity, both highly desirable to achieve the best CO₂ adsorption. 108

109	In the literature, only a few works investigated the production of ACs directly from the raw
110	giant reed (Bhattarai et al., 2022; Singh et al., 2017a; Singh et al., 2017b; Üner, 2019) while,
111	up to now, no study considered the AC production from this lignin stream originating from
112	such a biorefinery process. Moreover, in the literature, only two studies described the
113	adsorption performances of AC produced by giant reed for CO ₂ capture (Singh et al., 2017a;
114	Singh et al., 2017b). Based on all these considerations, the main objectives of the present
115	work were: (i) the preliminary characterisation of the starting precursor, namely the lignin-
116	rich residue; (ii) the optimisation of the thermochemical activation of this precursor to give
117	ACs with prevailing microporosity; (iii) the optimisation of the CO ₂ uptake and the evaluation
118	of the recycling of the most performing AC.

119

120 **2. Materials and methods**

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122 2.1 Biomass and reagents

123

Arundo donax L. was obtained from a mature 4-year-old plantation at the Centre for Agri-124 environmental Research "Enrico Avanzi" of the University of Pisa, located in San Piero a 125 Grado (Pisa, Italy). Culms and leaves were mixed and ground into particles of approximately 126 1.0 mm in size, then dried at 105 °C in an oven and stored in a desiccator until their 127 utilisation. All the used chemicals were provided by Sigma-Aldrich, with the following purity 128 degrees: water for HPLC, iron(III) chloride hexahydrate (>97%), sulfuric acid (98%), 129 hydrochloric acid (37%), potassium bromide (≥99%), sodium hydroxide (≥98%), potassium 130 hydroxide (90%). All reagents were used as received. 131

132

133 **2.2** Chemical composition of biomass samples

134

The chemical composition of the raw biomass and all the solid streams originating within the proposed biorefinery process was determined by the standard NREL methods (Sluiter *et al.*, 2008). Each sample was analysed three times.

138

139 2.3 Microwave-assisted catalytic conversion

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The Discover S-class microwave reactor (CEM company) was used to perform the twostep hydrolysis process of holocellulose. For the selective hydrolysis of hemicellulose to give xylose, catalysed by the homogeneous Lewis acid FeCl₃, the previously optimised reaction conditions were 1.5 wt% FeCl₃, 150 °C, 2.5 min, and 9 wt% of biomass loading (Di Fidio *et al.*, 2019). Subsequently, for the synthesis of levulinic and formic acid from the acidpretreated substrate, the previously optimised process conditions were 190 °C, 15 min, 2.2 wt% FeCl₃, and 9 wt% of biomass loading (Di Fidio *et al.*, 2019; Di Fidio *et al.*, 2020a).

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149 **2.4 Elemental analysis**

150

An automatic analyser Vario MICRO Cube (Elementar), equipped with a thermal conductivity detector, was used for the elemental analysis (C, H, N, S) of raw giant reed, lignin-rich residue, and AC samples. The oxygen content of the samples was calculated through the equation 1:

155
$$O(wt\%) = 100(wt\%) - (C(wt\%) + H(wt\%) + N(wt\%) + S(wt\%) + ash(wt\%))$$
 (1)

156

157 **2.5 Infrared spectroscopy**

A Perkin–Elmer "Spectrum Two" spectrophotometer was used for the acquisition of IR 159 spectra in transmission mode (KBr pellet method) and Attenuated Total Reflection (ATR) 160 mode. In the first case, 0.5 mg of sample was mixed with 400 mg of KBr. Then 120 mg of the 161 mixture was used for the preparation of the pellet having a thickness of $200 \pm 10 \mu m$. In the 162 second case, the same instrument was equipped with an attenuated total reflectance apparatus. 163 All the IR spectra were acquired through 24 scans in the range 4000-450 cm⁻¹ with a nominal 164 resolution of 8 cm⁻¹. ATR-FTIR was used for the characterisation of the raw material and 165 lignin-rich residue (our precursor of ACs), while the transmission mode (FTIR) was used for 166 the characterisation of ACs due to their very low transmittance. 167

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169 **2.6** Size-exclusion chromatography (SEC)

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SEC was performed on the soluble fraction of the lignin-rich residue (accounting for 67 wt%) in an alkaline solution (0.5 M NaOH), which was used as the solvent/eluent, according to the method proposed by Constant *et al.* (Constant *et al.*, 2016). Poly(styrene sulphonate) sodium salt standards (M_w range 891-258000 g/mol) were used for the calibration.

175

176 2.7 Synthesis of ACs

177

The DoE was performed according to the RSM, and it was exploited to optimise the AC synthesis from the lignin-rich residue. Activation temperature (A) and KOH/lignin weight ratio (B) were selected as the independent variables, namely the factors (Table 1). The reaction time was fixed at 60 min. For each factor, two levels (low and high) were selected, according to Table 1.

Factor	Name	Unit	Low	High
А	Temperature	°C	500	800
В	KOH/lignin	wt/wt	3	5

Table 1. Independent variables (factors) and levels of the experimental design.

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184

The responses (dependent variables) selected to monitor the AC synthesis were: i) AC yield (wt%); ii) carbon yield (wt%); iii) CO₂ uptake (mg/g). They were calculated by the following equations:

189	Y_{AC} (wt%) = (m _{AC} /m _{lignin}) × 100	(2)
190	$Y_C \text{ (wt\%)} = Y_{AC} \times (C\%_{AC}/C\%_{\text{lignin}})$	(3)
191	CO_2 uptake (mg/g) = m _{CO2} /m _{lignin}	(4)

where Y_{AC} is the AC yield, m_{AC} is the mass of recovered AC, m_{lignin} represents the mass of the lignin-rich residue, Y_C is the carbon yield, $C%_{AC}$ and $C%_{lignin}$ represent the carbon content in the AC and the lignin-rich residue, respectively, determined by elemental analysis, m_{CO2} is the mass of CO₂ determined by TGA in the adsorption tests.

For the AC synthesis, the lignin-rich residue (powder) was mixed with potassium 196 hydroxide flakes, by using an agate mortar. According to the B factor data of the DoE, 1 g of 197 the lignin-rich residue was mixed with a proper amount of KOH, until reaching a 198 homogenous solid mixture. For each run of the DoE, 1.25 g of the KOH/lignin mixture was 199 transferred into an alumina cup, which was subsequently placed in a tubular reactor and 200 heated under N₂ atmosphere (flow of 100 mL/min). The activation temperature was defined 201 according to each run of the experimental design. The heating/cooling rate of 5 °C/min was 202 adopted in all the tests. The solid stream recovered after pyrolysis was washed with 20 mL of 203 2 M HCl solution to remove the excess of KOH and with deionized water up to neutrality. AC 204 was dried at 105 °C up to constant weight and stored in a desiccator before its use. 205

206

207 **2.8 Thermogravimetric analysis (TGA)**

208

The TGA of the pristine precursor and the corresponding AC was carried out by using a 209 TGA Q500 TA Instrument. The alumina crucible containing ca. 10 mg of the sample was 210 dynamically heated, according to the following operating conditions: i) 20 °C/min from 30 to 211 105 °C under a constant flow of N₂ (100% v/v); ii) 105 °C for 10 min to determine the 212 humidity content of the sample; iii) 20 °C/min from 105 to 900 °C under a constant flow of 213 N₂ (100% v/v); iv) 900 °C for 10 min to determine the content of organic compounds; v) 214 cooling from 900 to 800 °C under an air/N₂ mixture flow (air 60% v/v, N₂ 40% v/v); vi) 800 215 °C for 20 min to determine the ash content and the fixed carbon content (by difference). 216

- 217
- 218 **2.9** CO₂ adsorption/desorption tests
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The CO₂ adsorption/desorption properties of ACs were evaluated using the TGA Q500, 220 TA Instrument. A schematic diagram of the experimental apparatus was reported in Figure 221 S1. The alumina crucible containing ca. 10 mg of the sample was dynamically heated under 222 the following operating conditions: i) 20 °C/min from 27 to 105 °C under a constant flow 223 (100 mL/min) of N₂ (100% v/v); ii) 105 °C for 10 min to remove the sample humidity; iii) 224 from 105 to 27 °C under a constant flow (100 mL/min) of N₂ (100% v/v). The adsorption test 225 was performed by treating the sample at 27 °C for 20 min under a 100 mL/min flow 226 containing CO₂ 60% v/v and N₂ 40% v/v. After reaching the plateau, the gas flow was 227 switched to 100 vol% N₂ (constant flow of 100 mL/min) and CO₂ desorption took place. Both 228 during adsorption and desorption tests, the sample weight variation was acquired as a function 229 of the time (Licursi et al., 2023). 230

232 2.10 Analysis of specific surface area, pore volume and size distribution

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Multi-point determination of specific surface area, pore volume and size distribution of AC 234 produced under different activation conditions was performed by ALFAST company. N2 235 adsorption/desorption isotherms were obtained at -196 °C by a 3Flex Adsorption Analyzer 236 (Micrometrics). Before the analysis, a pretreatment was conducted for 180 min at 200 °C 237 under a constant flow of N₂ (100% v/v), aimed at the humidity removal. The specific surface 238 area of each AC was determined through the Brunauer-Emmet-Teller (BET) method, while 239 the nonlocal density functional theory (NLDFT) was adopted for the determination of 240 micropore size distribution, according to the literature (Jagiello et al., 2015). The BET 241 specific surface area was evaluated taking into account the Rouquerol's theory (Rouquerol et 242 al., 2007), which is effective for extending BET analysis to microporous materials. In this 243 context, each microporous sample reveals an optimal range for the application of the BET 244 fitting. In the present study, the adopted range for ACs obtained in runs 3, 6 and under the 245 optimised conditions was withing 0.01-0.06 p/p^0 , whilst for the AC obtained in run 2, it was 246 0.02-0.15 p/p^0 . In all the performed analyses, the pressure ranges shifted downward from the 247 typical range of the BET method, namely $0.05-0.35 \text{ p/p}^0$, which is notoriously an unsuitable 248 range for microporous samples (Maziarka et al., 2021). Moreover, the Dubinin-Radushkevich 249 model was employed for the fitting of type I isotherms. 250

251

252 2.11 Scanning electron microscopy (SEM)

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For high-resolution imaging purposes, the SEM analysis was carried out by a FEI QUANTA 450 ESEM-FEG microscope, which operates in low vacuum mode, with a

chamber vacuum pressure ranging from 10-130 Pa. At 30 kV, it enables a nominal electron
beam resolution of 1.4 nm.

258

259 2.12 Raman spectroscopy analysis

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The lignin-rich residue and AC obtained under the optimised reaction conditions were analysed by Raman spectroscopy. Raman spectra were acquired by using a Renishaw inVia confocal micro-Raman system, connected to a Leica DLML microscope equipped with a NPLAN objective ($50\times$) having a numerical aperture of 0.75. The laser source was a Ng-YAG laser emitting at 532 nm, having a spectral resolution of 2.0 cm⁻¹. Positions of D and G band, FWHM and I_{DG} ratios were obtained by fitting and integrating the individual peaks with the Lorentzian function via OriginPro2023 software (R^2 value of fittings was higher than 0.98).

268

269 **3. Results and discussion**

270

271 **3.1** Characterisation of the AC precursor

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273 3.1.1 Analysis of chemical composition

The proposed fractionation route was developed according to a previously optimised approach, employing FeCl₃ as the acid catalyst and MW heating, as summarised in Figure 1 (Di Fidio *et al.*, 2019; Di Fidio *et al.*, 2020a). Inorganic salts are finding widespread use as green catalysts for the production of sugars, organic acids and/or furan derivatives from biomasses (Asada *et al.*, 2020; Loow *et al.*, 2015). Among them, FeCl₃ showed excellent catalytic performances for the production of monosaccharides, levulinic acid and 5hydroxymethylfurfural from lignocellulosic and starchy biomasses (Di Fidio *et al.*, 2020a; Iris

et al., 2017). The use of MW as the heating system improves the sustainability and efficiency of the proposed biorefinery scheme because it significantly reduces the reaction time and the energy consumption (Horikoshi *et al.*, 2017; Priecel and Lopez-Sanchez, 2018).

The chemical composition of the raw giant reed and the corresponding lignin-rich residue (constituting 21-23 wt% of the initial biomass weight, on a dry basis) obtained through the proposed two-step hydrolysis, is presented in Table 2.

287

Table 2. Chemical composition (wt%, on a dry basis) of raw *Arundo donax* L. and lignin-rich
residue, originating from the proposed two-step hydrolysis.

Fraction	Raw Arundo donax L.	Lignin-rich residue
Glucan	36.3	2.6
Xylan	17.3	-
Arabinan	1.9	-
Mannan	0.6	-
Acetyl groups	3.6	-
Ash	2.0	2.9
Extractives	13.5	-
Protein	1.9	1.3
Acid-insoluble lignin	22.0	93.2
Acid-soluble lignin	0.9	-

290

The final lignin-rich residue was characterised by an almost negligible cellulose content (ca. 202 2.5 wt%) and a high lignin content (ca. 93 wt%), confirming the efficiency of the proposed 203 catalytic approach for the selective cascade fractionation of the three main fractions of the 204 lignocellulosic biomass. 295

296 **3.1.2 ATR-FTIR spectroscopy**

ATR-FTIR spectroscopy (Fig. S2) corroborated the fractionation of the hemicellulose, 297 cellulose and lignin fractions. The absorption band at 3330 cm⁻¹ is due to the stretching of the 298 O-H group (Fiore et al., 2014), whose intensity reached its minimum in the lignin-rich 299 residue, according to the disappearance of the holocellulose and the chemical condensation of 300 aromatic structures characterising the lignin structure. The two absorption bands at 2920 and 301 2850 cm⁻¹ are due to the C-H stretching vibrations of -CH₂ / -CH₃ and O-CH₃, respectively 302 (Chen *et al.*, 2019). The absorption band at 1732 cm^{-1} is due to the C=O stretching vibrations 303 of unconjugated ketone, carbonyl, and ester groups and it is ascribable to the acetyl groups of 304 the hemicellulose fraction (Fiore et al., 2014). Its presence in the raw Arundo donax L. and its 305 absence in the lignin-rich residue confirmed the successful hydrolysis of the hemicellulose 306 component, as a consequence of the first hydrolysis step. Conversely, the absorption bands at 307 1701 and 1596 cm⁻¹, ascribed to the stretching of C=O conjugated to the aromatic rings of 308 lignin and to the aryl ring symmetric stretching of aromatic skeletal in lignin, respectively 309 (Chen et al., 2019), were sharper in the lignin-rich residue. Moreover, the absorption band at 310 1510 cm⁻¹ is assessed to the asymmetric aryl ring stretching, that at 1459 cm⁻¹ to the 311 asymmetric C-H deformation, that at 1210 cm⁻¹ to the C-C and C-O stretching, and that at 312 1110 cm⁻¹ to the aromatic C-H in-plane deformation (Di Fidio et al., 2020b). Lastly, C-O 313 stretching vibrations of hydroxyl and ether groups of cellulose are visible at 1033 cm⁻¹ (Fiore 314 et al., 2014). 315

316

317 3.1.3 Elemental analysis

The bulk removal of hemicellulose and cellulose from the *Arundo donax* L. biomass was also confirmed by elemental analysis. Data related to the raw biomass and the lignin-rich residue are reported in Table 3.

321

Table 3. Elemental analysis of raw *Arundo donax* L. and lignin-rich residue.

Daar		С	Н	Ν	0*	H/C	atomic	O/C	atomic
Run		(wt%)	(wt%)	(wt%)	(wt%)	ratio		ratio	
Raw A	rundo	46.4	5.8	0.3	45.4	1.5		0.7	
donax L.		40.4	5.8	0.5	43.4	1.5			
Lignin-rich r	esidue	62.0	4.8	0.2	28.6	0.9		0.3	

³²⁴

323

Carbon and oxygen contents of the lignin-rich residue were 62.0 and 33.0 wt%, respectively. These findings are consistent with previously reported literature data for major commercial lignin types, including Kraft lignin Indulin[®] AT, Soda Protobind[™] 1000, and Alcell[™] organosolv lignin (Constant *et al.*, 2016).

329

330 3.1.4 SEC of the alkaline-soluble lignin

The molecular weight of the lignin-based precursor can significantly influence the pore ordering of the obtained AC (Qin *et al.*, 2018). The molar mass distribution of the alkalinesoluble fraction of the lignin-rich residue (67 wt%) was determined by SEC (Fig. S3). The number average molecular weight (M_n) was 804 g/mol, while the weight average molecular weight (M_w) was 2252 g/mol. The polydispersity index (M_w/M_n) was 2.8, thus indicating a broad distribution of the biopolymer chains. These results agreed with those previously reported for *Arundo donax* L.-derived lignins (You *et al.*, 2013) as well as for other

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ιn

commercial lignins (Constant *et al.*, 2016). Remarkably, such alkaline-soluble lignin fraction
could be separately exploited for the synthesis of even more added-value bio-carbons, such as
ordered mesoporous carbons, by soft-template methods (Qin *et al.*, 2018), opening the way to
further valorisation routes of this residue towards various valuable chemicals and materials.

342

343 **3.2** Synthesis and characterisation of AC starting from the lignin-rich residue

344

According to the literature, several activation methods are available, including steam 345 activation and carbonisation coupled with gas activation, considered as physical activation 346 methods, or chemical activation ones, requiring the impregnation with a chemical activating 347 agent, such as KOH, H₃PO₄, ZnCl₂ (Azmi et al., 2022; Malini et al., 2023). There are also 348 studies on MW-assisted activation, such as MW-assisted pyrolysis and hydrothermal 349 carbonisation (HTC) (Kaur et al., 2021; MacDermid-Watts et al., 2021). All these methods 350 can lead to ACs with different surface properties (mainly in terms of specific surface area and 351 pore size distribution) and chemical composition. The choice of the most appropriate 352 activation method depends on several factors: first of all, the final application of the AC and, 353 secondly, the kind of the precursor (Licursi et al., 2023). In the present work, the lignin-rich 354 residue was used as the precursor to produce cheap AC, resulting in efficient CO₂ adsorption. 355 KOH activation is effective for the synthesis of microporous AC with a high capacity for CO₂ 356 adsorption (Nandi et al., 2023; Singh et al., 2017a). In this context, ACs from KOH activation 357 are characterised by a high surface area and narrow pore size distribution (Malini et al., 2023; 358 Xing et al., 2023). The solid-to-solid reaction is effective for avoiding the carbonatation of 359 KOH, but also for economical and practical reasons. In particular, when KOH reacts with 360 carbon of biomass, K₂CO₃, K, H₂O, H₂, CO₂ and CO are produced, according to the following 361 reactions (Malini et al., 2023; Nandi et al., 2023): 362

- $363 \qquad C_{(s)}+2KOH_{(s)}+H_2O_{(l)} \rightarrow K_2CO_{3(s)}+2H_{2(g)}$
- $364 \qquad 2C_{(s)} + 6KOH_{(s)} \rightarrow 2K_2CO_{3(s)} + 2K_{(s)} + 3H_{2(g)}$
- $365 \qquad 2C_{(s)} + 2KOH_{(s)} \rightarrow 2CO_{(g)} + 2K_{(s)} + H_{2(g)}$
- $366 \qquad 2C(s)+3H_2O(l) \rightarrow 2CO(g)+6H_2(g)+2CO_2(g)$
- $367 \qquad C_{(s)} + CO_{2(g)} \rightarrow 2CO_{(g)}$
- $368 \qquad 2KOH_{(s)} \rightarrow K_2O_{(s)} + H_2O_{(g)}$
- $369 \qquad KOH_{(s)} + CO_{2(g)} \rightarrow K_2CO_{3(s)} + H_2O_{(g)}$
- The production of volatiles from the precursor contributes to improve the AC porosity. In addition, the formation of pores is favoured by the following reactions, occurring mainly between biomass carbon and K_2CO_3 or K_2O (Nandi *et al.*, 2023):

373
$$K_2CO_{3(s)} + 2C_{(s)} \rightarrow 2K_{(s)} + 3CO_{(g)}$$

374
$$K_2CO_{3(s)} + 2C_{(s)} \rightarrow K_2O_{(s)} + 2CO_{(g)}$$

$$375 \qquad K_2O_{(s)}+C_{(s)} \rightarrow 2K_{(s)}+2CO_{(g)}$$

A chemometric approach based on the RSM was adopted to optimise the main process parameters of the lignin activation step (Table 4). The experimental (full-factorial randomised) test plan is shown in Table 4, including 10 total runs, with 4 runs at factorial points, 4 runs at axial points, and 2 replicates at the central point of the design, according to equation 5:

$$381 N_{\rm runs} = 2^n + 2n + n_{\rm c} (5)$$

where N_{runs} is the number of total experimental runs required for a full-factorial central composite design (CCD), *n* is the number of independent factors, 2n is the number of axial runs and n_c is the number of runs conducted at the centre of the design. The CCD alpha value (*a*), which represents the distance of axial points from the centre of the design space, was set to 1.414 to obtain a rotatable design (Table 4).

Run	T (°C)	KOH/lignin weight ratio (wt/wt)
1	862.1	4.0
2	800.0	3.0
3	650.0	2.6
4	800.0	5.0
5	437.9	4.0
6	500.0	3.0
7	650.0	5.4
8	650.0	4.0
9	500.0	5.0
10	650.0	4.0

Table 4. Experimental design matrix (process time 60 min).

389

388

The TGA curves of the precursor and ACs were acquired (Fig. S4) while the corresponding proximate analysis data are reported in Table 5.

Table 5. Proximate analysis data of precursor and ACs.

Run	Volatiles (wt%)	Fixed carbon (wt%)	Ash (wt%)
Lignin-rich residue	55.3	40.3	4.4
1	7.9	78.1	14.0
2	19.6	62.3	18.1
3	28.0	66.9	5.1
4	9.2	86.3	4.5
5	35.8	55.6	8.6
6	37.4	58.7	3.9

Journal Pre-proof						
7	14.8	74.0	11.2			
8	23.4	71.3	5.3			
9	50.7	42.6	6.7			
10	20.5	74.3	5.2			

³⁹⁴

All the ACs produced under less severe conditions (≤ 500 °C), such as those obtained from 396 run 5 (437.9 °C, 4.0 KOH/lignin), run 6 (500 °C, 3.0 KOH/lignin) and run 9 (500 °C, 5.0 397 KOH/lignin), showed the lowest fixed carbon content, which was comparable with that of the 398 pristine lignin-rich residue (40 wt%). On the contrary, ACs synthesised at higher temperatures 399 $(\geq 650 \text{ °C})$ were characterised by a higher content of fixed carbon, confirming the advanced 400 carbonisation of the lignin-rich precursor. Moreover, most of the ACs showed a lower ash 401 content than the maximum one (10 wt%) allowed for commercial uses (Zulkania et al., 2018). 402 The results of the elemental analysis of all the AC samples were reported in Table 6. 403

405	Table 6. Elementa	analysis data	a of lignin-rich	residue and	synthesised ACs
405		anarysis uau	a of fightin-field	icsiduc allu	synthesiscu ACs.

	С	Н	N	0*	H/C	atomic	O/C	atomic
Run	(wt%)	(wt%)	(wt%)	(wt%)	ratio		ratio	
Lignin-rich residue	62.0	4.8	0.2	28.6	0.9		0.3	
1	77.6	0.9	0.3	7.3	0.1		0.1	
2	76.0	0.4	0.4	5.1	0.1		0.1	
3	73.0	3.2	0.1	18.6	0.5		0.2	
4	82.4	0.8	0.2	12.1	0.1		0.1	
5	59.3	2.8	0.1	29.2	0.6		0.4	
6	72.6	3.1	0.1	20.3	0.5		0.2	

³⁹⁵

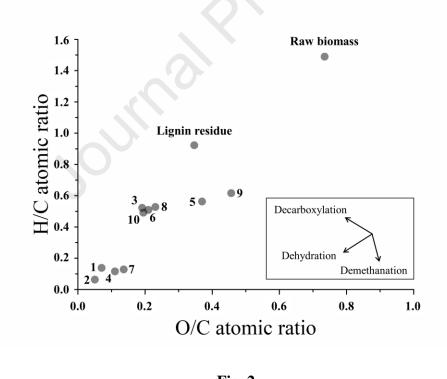
Journal Pre-proof						
7	74.3	0.8	0.2	13.5	0.1	0.1
8	70.0	3.1	0.1	21.5	0.5	0.2
9	56.1	2.9	0.1	34.1	0.6	0.5
10	72.8	3.0	0.1	18.9	0.5	0.2

 $406 \quad * O(wt\%) = 100(wt\%) - (C(wt\%) + H(wt\%) + N(wt\%) + S(wt\%) + ash(wt\%))$

407

The H/C and O/C atomic ratios were reported in the van Krevelen diagram, which is useful for depicting the progress of the carbonisation progress, highlighting some details about the corresponding mechanism (Fig. 2).

411



412 413

Fig. 2

The distribution of the H/C and O/C atomic ratios in the Van Krevelen diagram demonstrated that dehydration reaction was the prevailing path involved in the production of both ligninrich residue and ACs. The ACs obtained at high temperatures (≥ 650 °C) were characterised

by lower H/C and O/C atomic ratios, while those obtained under less severe conditions (\leq 500 °C), such as ACs obtained from runs 5 and 9, showed higher O/C values. FTIR spectra of ACs obtained in runs 1-10 were acquired (Fig. S5). The absorption band in the range of 3100-3500 cm⁻¹ is ascribable to the stretching of the O-H bonds. Those in the range 2800-3000 cm⁻¹ are related to the C-H stretching vibrations of -CH₂ and -CH₃ groups.

The absorption bands in the range 1000-1300 and 1640-1750 cm⁻¹ are due to the stretching vibrations of C-O and C=O bonds of ketones, aldehydes and carboxylic acids, as well as phenolic esters. The intensity decrease of such absorption bands is related to the occurred removal of volatile organic compounds and the deoxygenation of the pristine material. The band at 1630 cm⁻¹ is due to C=C ring stretching vibrations and it is indicative of progress of the biomass carbonisation.

The CO₂ uptake of the starting lignin-rich residue, namely the control test, and of the ACs 429 obtained in the runs 1-10 was evaluated (Fig. S6). The AC characterised by the highest CO₂ 430 uptake (72.6 mg/g) was obtained from run 3 (650.0 °C, KOH/lignin 2.6 wt/wt, 60 min). 431 Moreover, by comparing the CO₂ adsorption uptake of the pristine lignin-rich residue (6.9 432 mg/g) and the AC, it becomes clear that the activation process significantly improved the 433 adsorption performance. Furthermore, the use of temperatures higher than 800 °C or lower 434 than 500 °C, together with high activating agent ratios (≥ 4 wt/wt), led to lower CO₂ uptakes 435 (runs 1, 4, 5, 9, Table 6). Based on these results, intermediate activation temperatures and low 436 KOH/lignin weight ratios were effective in improving the CO₂ uptake capacity of the ACs. 437 Table 7 summarised the values of each response variable achieved in all the runs performed in 438 the RSM analysis. 439

440

441

Table 7. Experimental data of selected response variables.

Run

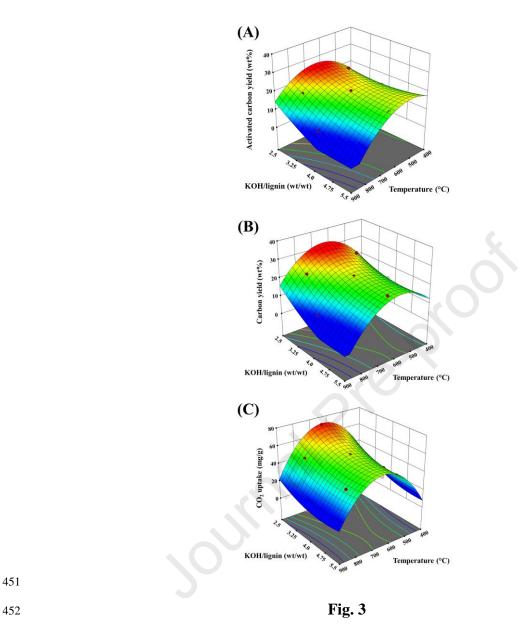
AC yield (wt%) Carbon yield (wt%) CO₂ uptake (mg/g)

Control [*]	-	-	6.9
1	6.4	8.0	17.4
2	18.3	22.4	47.0
3	25.6	30.1	72.6
4	6.2	8.2	40.0
5	16.3	15.6	27.8
6	22.1	25.8	48.9
7	18.2	21.9	49.5
8	20.5	23.1	55.2
9	19.2	17.4	36.3
10	19.0	22.3	54.3

^{442 *} Control test: pristine lignin-rich residue.

443

A mathematical model was obtained for each response variable describing the experimental domain. All the obtained models were characterised by a regression square value (R^2) higher than 0.96 and a not-significant Lack of Fit (*p*-value > 0.1). The analysis of variance (ANOVA) was performed, and corresponding data were reported in Tables S1-3. Figure 3 shows the 3D surfaces for AC and carbon yields and CO₂ uptake, respectively, as a function of the investigated process conditions.



453

The coded model equations related to the AC yield (wt%), carbon yield (wt%) and CO₂ uptake (mg/g) are the following:

456
$$Y_{AC}(wt\%) = 19.75 - 3.85 \times A - 3.18 \times B - 2.30 \times A \times B - 4.24 \times A^2 + 1.03 \times B^2$$
 (6)

457
$$Y_{C}(wt\%) = 22.70 - 2.92 \times A - 4.27 \times B - 1.45 \times A \times B - 5.56 \times A^{2} + 1.54 \times B^{2}$$
 (7)

458
$$Y_{CO2} (mg/g) = 54.75 - 1.61 \times A - 6.53 \times B + 1.40 \times A \times B - 15.77 \times A^2 + 3.46 \times B^2$$
(8)

The prediction of the optimal process conditions was subsequently carried out, aimed at simultaneously maximising the AC yield, the carbon yield, and the CO₂ uptake. The predicted

optimal conditions were found, corresponding to an activation temperature of 630 °C and a
KOH/lignin weight ratio of 3.0 wt/wt. Under these conditions, the model predicted the AC
yield of 24.1 wt%, the carbon yield of 28.6 wt% and the CO₂ uptake of 64.9 mg/g (6.5 wt%).
These results were experimentally validated, obtaining an AC yield of 34.4 wt%, a carbon
yield of 40.6 wt% and a promising CO₂ uptake of 72.3 mg/g (7.2 wt%), confirming the
effectiveness of the proposed model.

According to Song *et al.* (Song *et al.*, 2015), commercial AC is characterised by a CO₂ adsorption capacity of around 65 mg/g (6.5 wt%) at 1 bar and 25 °C, while biomass-derived ACs show wider CO₂ uptakes, reasonably in the range 49-210 mg/g (Serafin *et al.*, 2017). Thus, our AC produced from the *Arundo donax* L. lignin-rich residue, within the proposed biorefinery scheme, can be advantageously exploited for this application.

472 Raman spectra of starting lignin-rich residue and AC obtained under the optimised reaction
473 conditions were acquired (Fig. 4).

474

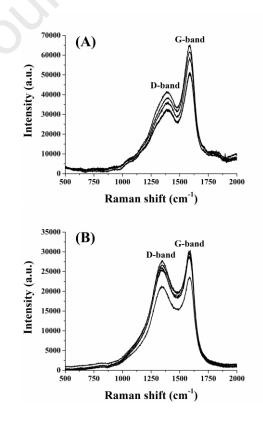


Fig. 4

477

Raman spectra of disordered and amorphous carbon exhibit two peaks at around 1340-1360 cm⁻¹ (D-band) and 1570-1600 cm⁻¹ (G-band), reflecting the defects in the samples and the ordered sp² carbon plane, respectively. The intensity ratio of the D and G band (I_{DG}) is generally considered indicative of the disorder and the graphitization degree of the carbonaceous material, whereas the values for the FWHM reflect the sizes of the domains of the different kinds of carbon structure (Yagmur *et al.*, 2020). The parameters of interest for each deconvoluted spectrum were reported in Table 8.

485

Table 8. Measured and calculated data from Raman analysis (arithmetic mean value ±
standard deviation).

	Sample	D pos (cm ⁻¹)	G pos (cm ⁻¹)	IDG	FWHMD	FWHM _G
	Lignin-rich residue	1378±5**	1587±3	0.64±0.02**	248±8*	104±2**
	AC	1347±3**	1588±6	0.97±0.02**	264±4*	95±3**
488	*p<0.01; **p<0.001	5				

489

The synthesised AC showed a higher I_{DG} value than that of the lignin-rich residue, suggesting 490 the presence of more defects and a disordered graphite-like structure (i.e., a lower 491 graphitization degree). Such a structure may be due to the intercalation of potassium and/or to 492 the presence of oxygenated functional groups. Raman spectra of AC exhibited a strong signal 493 for the D-mode at a decreasing position with respect to the pristine lignin-rich residue, which 494 further confirms the disordered structure of this carbonaceous material. Higher FWHM of the 495 D band was observed for AC, again highlighting its disordered texture. G-band FWHM is 496 often employed to characterise carbon crystallites, and a narrower G-band FWHM implies a 497

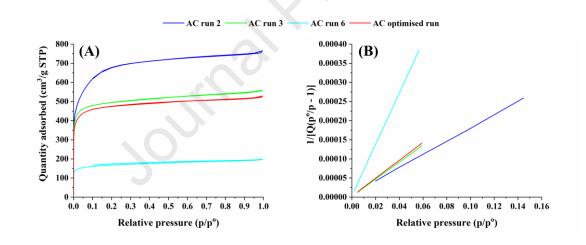
- ⁴⁹⁸ reduced presence of bond angle disorder in sp^2 carbons.
- 499

500 **3.3** Analysis of specific surface area, pore volume and size distribution

501

⁵⁰² N₂ adsorption isotherm linear plot and BET specific surface area plot at -196 °C of ACs ⁵⁰³ obtained from run 2 (800 °C, KOH/lignin 3.0 wt/wt, 60 min), run 3 (650 °C, KOH/lignin 2.6 ⁵⁰⁴ wt/wt, 60 min), and run 6 (500 °C, KOH/lignin 3.0 wt/wt, 60 min), corresponding to the ⁵⁰⁵ lowest, the intermediate and the highest temperature selected in the DoE, were compared in ⁵⁰⁶ Figure 5. Moreover, they were compared with the AC synthesised under the optimised ⁵⁰⁷ reaction conditions (630 °C, KOH/lignin 3.0 wt/wt, 60 min).

508



509 510

Fig. 5

511

KOH activation promoted the selective formation of micropores, as confirmed by the type I isotherms of these ACs (Fig. 5). AC produced in the run 2 (800 °C, KOH/lignin 3.0 wt/wt) was characterised by significant microporosity and very high specific surface area, that was 2507.4 m²/g. This specific surface area was composed of a micropore area of 2369.4 m²/g and an external surface area of 138.0 m²/g. AC obtained from the run 3 (650 °C, KOH/lignin 2.6 wt/wt) was also characterised by a microporous texture, with a specific surface area of 1940.4 26

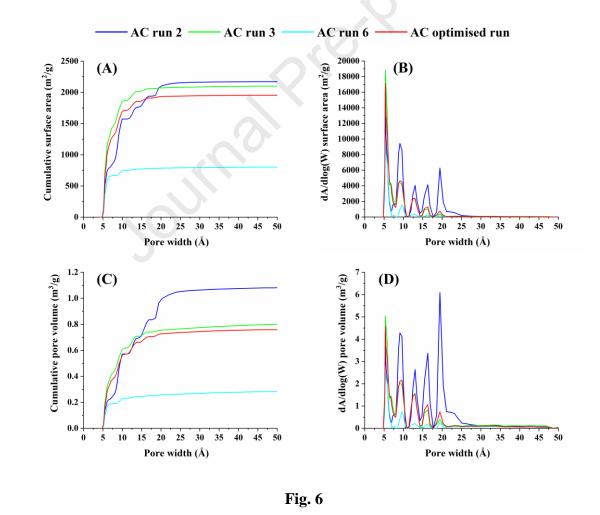
 m^2/g , whereas the micropore area was 1817.1 m^2/g and the external surface area was 123.3 518 m²/g. The specific surface area of AC from run 6 (500 °C, KOH/lignin 3.0 wt/wt) was only 519 $645.9 \text{ m}^2/\text{g}$, whereas the micropore area was $587.4 \text{ m}^2/\text{g}$ and the external surface area was 58.5520 m^2/g . These results confirmed that the synthesis of ACs with high microporosity is favoured 521 by higher temperatures, in agreement with the literature (Azmi et al., 2022). The main 522 parameters affecting the microstructure of ACs and, consequently, the N_2 gas sorption results 523 are the type of activating agent, the impregnation ratio, and the activation temperature (Azmi 524 et al., 2022). Regarding the activating agent, the dissolution of ether linkages of lignin-rich 525 materials is facilitated by the utilisation of alkaline chemicals (Malini et al., 2023). Moreover, 526 the application of an activating agent containing potassium generates additional micropores, 527 exploiting the capacity of potassium for expanding the carbon layers. Consequently, this 528 process enhances pore accessibility by breaking down longer fibers, favouring the production 529 of ACs characterised by very high specific surface area and a more uniform distribution of 530 micropores (Singh et al., 2017a). Regarding the impregnation ratio, a reduced concentration 531 of KOH enables a more controlled and stable elimination of volatile matter while preventing 532 the deposition of tar, thus resulting in a greater abundance of micropores (Azmi et al., 2022). 533 Finally, the temperature employed during the activation process of carbon materials plays a 534 crucial role in determining the pore volume, the distribution of pore sizes, the development of 535 microporosity, and the overall specific surface area. Generally, higher temperatures facilitate 536 the removal of moisture and volatile components from the precursor, promoting the further 537 creation of pores (Azmi et al., 2022). However, by increasing the temperature, there is an 538 expected significant decrease in the AC yield, along with the higher concentration of ashes, as 539 reported in Tables 5 and 7. 540

541 Under the optimised reaction conditions (630 °C, KOH/lignin 3.0 wt/wt), AC showed the 542 specific surface area of 1848.0 m²/g, whereas the micropore area was 1762.8 m²/g and the

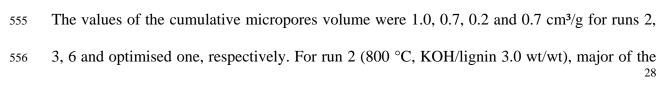
external surface area was 85.2 m²/g. As expected, these results were quite similar to those achieved from run 3. The specific surface area of 1848.0 m²/g was significantly higher than those obtained for ACs from unpretreated *Arundo donax* L., within the range 500.0-1568.0 m²/g (Ahmed, 2016; Singh *et al.*, 2017a). The high specific surface area obtained in the present work further demonstrates the effectiveness of our approach.

Figure 6 shows the cumulative surface area, the dA/dlog(W) surface area, the cumulative pore volume and the dV/dlog(W) pore volume as a function of the pore width of AC obtained from runs 2, 3, 6 and DoE validation run.

551







micropores was characterised by a width of 9.2, 13.0 and 16.2 Å while the presence of larger 557 micropores of around 19 Å was ascertained, as shown in Figures 6B and 6D. For run 3 (650 558 °C, KOH/lignin 2.6 wt/wt), the most abundant micropores showed a width of 5.2, 9.1 and 559 13.0 Å. The AC produced in run 6 (500 °C, KOH/lignin 3.0 wt/wt) presented micropores of 560 5.3 and 9.6 Å. Lastly, AC obtained under the optimised reaction conditions (630 °C, 561 KOH/lignin 3.0 wt/wt) was characterised by micropores with a width of 5.2, 9.1 and 13.0 Å, 562 confirming the similar microporous structure and pore distribution of AC of run 3. Moreover, 563 the micropores volume $(0.7 \text{ cm}^3/\text{g})$ was significantly higher the those reported in the literature 564 for AC obtained from Arundo donax L., ranging from 0.2 to 0.5 cm³/g (Ahmed, 2016; Singh 565

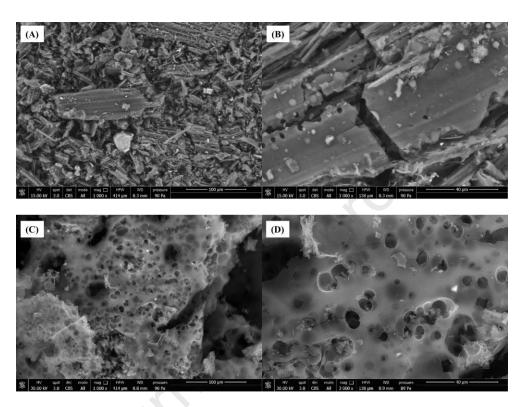
et al., 2017a), demonstrating again the effectiveness of the proposed cascade process.

The improvement of the CO₂ uptake requires the enhancement of the microporosity, 567 surface area, and pore volume of the AC. Moreover, AC readily lends itself to the 568 incorporation of surface oxygenated functional groups like carboxylates and hydroxyls, 569 enabling CO_2 capture through processes such as cation exchange, strong complexation, and 570 electrostatic attractions (Azmi et al., 2022). Remarkably, heteroatoms such as sulphur, 571 nitrogen, oxygen, and hydrogen assume a crucial role by interacting specifically with CO₂, 572 573 leading to improved CO₂ selectivity, and aiding in gas separation. Doping AC with oxygen or utilising raw materials rich in oxygen as precursors facilitates the creation of hydroxyl, 574 carboxylic, and phenol functional groups, which in turn promote CO₂ capture. At the same 575 time, a high concentration of metal oxides can result in pore clogging, ultimately diminishing 576 the performance of CO₂ adsorption (Azmi et al., 2022). Moreover, pores below 10 Å exhibit 577 remarkable selectivity for CO₂ molecules, when present in a N₂/CO₂ mixture (Abd et al., 578 2021). This selectivity arises from their ability to effectively block the passage of N₂ 579 molecules through the pore walls. However, pores with dimensions lower than 3.5 Å show 580 reduced adsorption performance because they approach the kinetic diameter of CO₂ molecules 581

(3.3 Å). On the other hand, pores exceeding 10 Å in size are unsuitable for low-pressure CO₂ 582 capture, since they may not achieve a sufficiently dense packing of CO₂ molecules (Abd et 583 al., 2021). Once having verified the possibility of obtaining AC with a tailored microporosity, 584 it could be possible to further improve its surface properties, depending on the physico-585 chemical properties of the component to be adsorbed on it. Based on these considerations, the 586 results obtained from the analysis of the specific surface area, pore volume and size 587 distribution of ACs produced in runs 2, 3, 6 and under the optimised conditions (Fig. 5 and 6) 588 were correlated with those obtained from the analysis of CO₂ uptake (Table 7), as well as with 589 those obtained from the elemental analysis (Table 6). The AC produced in run 2 (800 °C, 590 KOH/lignin 3.0 wt/wt) was characterised by the highest values of specific surface area, 591 micropore area, external surface area and cumulative micropores volume, but also by a lower 592 CO₂ uptake (47.0 mg/g) with respect to the values achieved for ACs produced in run 3 (650 593 °C, KOH/lignin 2.6 wt/wt) and under the optimised reaction conditions (630 °C, KOH/lignin 594 3.0 wt/wt), equal to 72.6 and 72.3, respectively. The better adsorbing performances of these 595 last two ACs can be explained by considering the micropore size and distribution (Fig. 6), as 596 well as the oxygen content (Table 6). In fact, ACs produced in run 3 and under the optimised 597 conditions were characterised by the abundance of micropores with a width of 5.2, 9.1 and 598 13.0 Å and by the oxygen content of 18.6 and 18.3 wt%, respectively. Differently, AC 599 produced in run 2 was mainly characterised by larger micropores with a width of 13.0, 16.2 600 and 19 Å and by a lower oxygen content (5.1 wt%) and higher ash content (18.1 wt%). The 601 synergistic effect of these features decreased the selectivity of AC obtained in run 2 and 602 increased that of ACs produced in run 3 and in the optimised run towards the adsorption of 603 CO₂ molecules in the mixture CO₂/N₂, according to the literature (Abd et al., 2021). 604 According to this reasoning, a schematic representation of the CO₂ adsorption mechanism was 605 reported in Figure S7. 606

SEM images of pristine lignin-rich precursor and AC obtained under the optimised process
conditions (630 °C, KOH/lignin 3.0 wt/wt, 60 min) are shown in Figure 7.

609



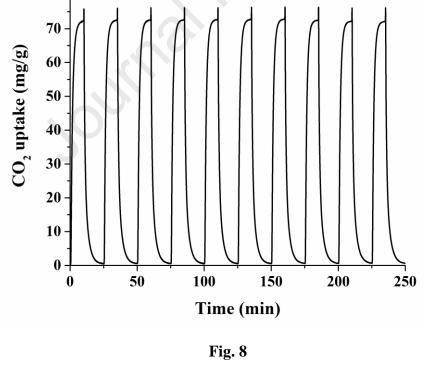
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The effect of the thermochemical activation was evident since the lignin-rich residue was 613 characterised by a non-porous and flat morphology while AC revealed a rather porous and 614 shrunk structure, with pores diameter <40 µm (Fig. 7D). Moreover, as shown in Fig. 7C, AC 615 was characterised by a uniform distribution of micropores. The morphological features of AC 616 obtained under the optimised process conditions were ascribed to a collapse of the carbon 617 matrix, due to the higher amount of KOH used in the activation protocol (KOH/lignin ratio of 618 3.0 wt/wt), in agreement with the literature findings (Singh et al., 2017a). The high 619 concentration of KOH initiates the carbon walls' breakdown, interconnecting an aligned 620 porous carbon structure, through oxidation at high temperature. Simultaneously, potassium 621 residues produced during the activation process profoundly alter the surface morphology of 622

623	the sample (Nandi et al., 2023). These findings underscored the importance of properly tuning
624	the activation process of ACs, characterised by a uniform morphology, a consistently aligned
625	porous structure, and outstanding surface properties, such as a high specific surface area and
626	micropore volume.
627	
628	3.4 Recycling test of activated carbon for CO_2 uptake
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630	Figure 8 shows 10 adsorption and desorption cycles of CO ₂ by the AC obtained under the
631	optimised process conditions.
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	$\widehat{\mathbf{n}}$
	ୁଇଁ ⁶⁰



- 633 634
- 635

Firstly, it is noteworthy that the maximum achieved CO_2 uptake of 72.3 mg/g was obtained by working at a CO_2 partial pressure of 0.60 bar, which is more representative of more real conditions, such as those of post-combustion flue gas. This adsorption performance

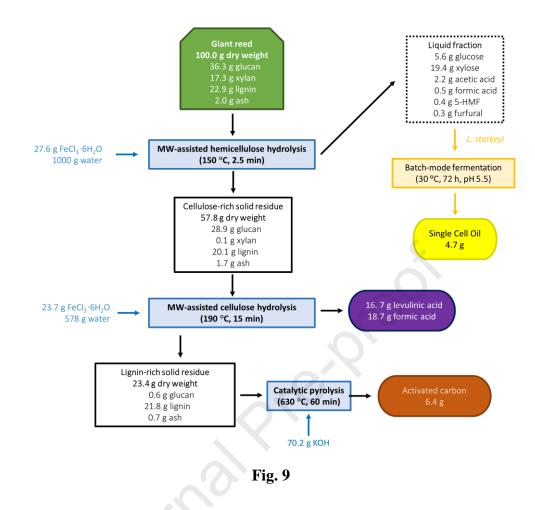
demonstrated the feasibility of the use of this kind of AC as CO₂ adsorbent for industrial 639 applications. Moreover, the equilibrium time observed in the recycling tests was always very 640 short (ca. 10 min), confirming the good properties and performances of this biomaterial. 641 Lastly, an almost identical trend was ascertained for all the cycles, thus demonstrating that the 642 AC obtained in this study is regenerable and reusable, which are desirable aspects for eventual 643 industrial uses. The prevailing presence of microporosity in the synthesised AC is also 644 desirable for performing solid-liquid adsorption studies, for example, those aimed at the 645 removal of organic pollutants, such as phenol, from wastewaters (Dehmani et al., 2023). On 646 this basis, the use of the synthesised AC for such applications in the liquid phase seems 647 promising and certainly worthy of further attention. These important features significantly 648 increased the sustainability of the implemented approach for the lignin residue valorisation, 649 especially when AC finds application as filter material (Sevilla et al., 2012). 650

651

652 **3.5** Flow diagram of the proposed biorefinery scheme

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Figure 9 shows the mass flow diagram of the proposed biorefinery scheme, which is based on the MW-assisted conversion of hemicellulose and cellulose into xylose and levulinic acid, respectively. The subsequent step involves upgrading the xylose-rich hydrolysate (XRH) to produce single cell oil (SCO) using the yeast *L. starkeyi*, as discussed in our previous works (Di Fidio *et al.*, 2019; Di Fidio *et al.*, 2020a; Di Fidio *et al.*, 2021a). Finally, the lignin-rich stream is valorised by producing AC under the optimised process conditions presented in this study.



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Starting from 100 g of Arundo donax L., 19.4 g of xylose, 5.6 g of glucose, 16.7 g of 665 levulinic acid and 18.7 g of formic acid were produced. Then, by fermenting the XRH, 4.7 g 666 of SCO was achieved. Moreover, a final lignin-rich stream (23 g), containing 93.2 wt% acid-667 insoluble lignin, was obtained as the residue of this process, which allows the production of 668 6.4 g of AC. Lastly, it is important to emphasise the short processing time of the entire 669 biorefinery process proposed in the present study since the first step requires only 2.5 min, the 670 second one 15 min and the last one 60 min. The complete valorisation of the starting raw 671 material and the sustainable reaction conditions adopted in each step significantly improved 672 the sustainability of the cascade process in the perspective of the Green Chemistry principles. 673

674

675 Conclusions

A new thermochemical route was optimised for closing the cycle of the valorisation of 677 Arundo donax L. After the hydrolysis of hemicellulose to xylose and cellulose to levulinic 678 and formic acid, the final lignin-rich residue was characterised and chemically activated by 679 KOH to produce AC, which was exploited for CO₂ adsorption. The chemometric approach 680 was chosen to improve the activation protocol. Under the optimised conditions (630 °C, 681 KOH/lignin 3.0 wt/wt, 60 min) the AC yield was 34.4 wt% and the maximum CO₂ uptake 682 was 72.3 mg/g, kept over 10 cycles of adsorption/desorption tests, demonstrating its feasible 683 regeneration without losing its starting CO₂ uptake capacity. The complete and tailored 684 conversion of the different components of this non-edible biomass represents a step forward 685 in the perspective of green and sustainable biorefinery processes. 686

687

688 Acknowledgements

689

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702 Appendix A. Supplementary data

- E-supplementary data of this word can be found in online version of the paper.
- 704

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Highlights

- The biorefinery of lignocellulosic Arundo donax L. biomass was completed. •
- Microporous activated carbon was obtained from the residual lignin-rich fraction. •
- A chemometric approach was used to optimise the production of activated carbon. ٠
- Yields in activated carbon and carbon were 34.4 and 40.6 wt%, respectively. •
- The CO₂ uptake was 7.2 wt%, kept over 10 cycles of adsorption/desorption. •

CRediT authorship contribution statement

Nicola Di Fidio: Conceptualization, Methodology, Investigation, Formal analysis, Writing - original draft. Domenico Licursi: Formal analysis, Writing - review & editing. Monica Puccini:
Conceptualization, Methodology, Formal analysis, Writing - review & editing, Funding acquisition.
Sandra Vitolo: Writing - review & editing, Resources. Anna Maria Raspolli Galletti: Writing - review & editing, Supervision, Funding acquisition.

Declaration of interests

☑ The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

□ The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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