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Tunable Production of Diesel Bio-blendstock by Rhenium-catalyzed Hydrogenation of Crude Hexanoic Acid from Grape Pomace Fermentation

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Abstract: The transition from fossil resources to renewable ones represents a pressing need. The 16 acidogenic fermentation of biomass-derived ethanol to carboxylic acids represents a novel and 17 smart possibility, opening the way to the production of even more value-added bio-products 18 through cascade chemical approaches. In this work, the hydrogenation of commercial hexanoic 19 acid to give 1-hexanol/hexyl hexanoate mixtures was preliminary studied in the presence of com-20 mercial rhenium catalysts (Re₂O₇ and 5 wt% Re/C), which resulted active and selective mainly to-21 wards 1-hexanol. On the other hand, the use of niobium phosphate as the acid co-catalyst markedly 22 shifted the selectivity towards hexyl hexanoate. 5 wt% Re/C and physical mixtures of [5 wt% Re/C + 23 niobium phosphate] were further tested for the hydrogenation of crude hexanoic acid obtained by 24 fermentation of white grape pomace, confirming the promising performances of these catalytic 25 systems and their recyclability. For the first time, the employ of 1-hexanol/hexyl hexanoate mix-26 tures as diesel blendstock has been evaluated, highlighting a significant reduction of the soot and 27 CO emissions, without any significant change in the engine performance. The promising properties 28 of these oxygenated additives are favorable to the partial replacement of traditional fossil fuels, in 29 accordance with the short-term goals of the EU countries. 30

Keywords: Grape pomace; Carboxylic acids; Rhenium catalysts; Hydrogenation; Diesel blendstock 31

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1. Introduction

Biomass represents a key feedstock in the transition from fossil resources to re-34 newable ones to synthesize new biofuels and bio-chemicals through biological and/or 35 chemical pathways_[1]. The use of nonedible feedstocks is strategic for these goals 36 without creating any pressure on land use and hindering the food supply [2]. In this 37 perspective, grape pomace, an abundant agro-industrial waste deriving from the wine-38 making process, is a promising feedstock to develop a bio-refinery approach. About 9 Mt 39 of grape pomace are globally produced every year, these are valorized in centralized 40 bio-refineries that obtained anthocyanins, polyphenols, tartaric acid but most of all dis-41 tilled ethanol (e.g. for biofuel) [3]. Remarkably, ethanol distillation is an energy intensive 42 process, e.g. 22% of the ethanol contained energy is consumed in the recovery process [4]. 43 So far, the economic sustainability of grape pomace ethanol distillation had been based 44 on subsidies from the government to distilleries. In the framework of the so-called safety 45

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Copyright: 2022by the authors. Submitted for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (https://creativecommons.org/license s/by/4.0/). and sustainable by-design, an alternative route for ethanol valorization could represent 46 an improvement towards a circular economy or could represent a growth of the chemical 47 portfolio in any case. In this line, the production of hexanoic acid from the ethanol con-48 tained in red grape pomace was recently reported: the anaerobic fermentation of grape 49 pomace under chain elongation conditions (25 g/L of hexanoic acid) and a consecutive 50 simple down-stream procedure allowed obtaining ca. 90% pure hexanoic acid [5]. Such 51 valorization represents an evolution of the carboxylate platform state-of-the-art, i.e. 52 demonstrating the potential industrial technical feasibility through a proof-of-concept. In 53 fact, hexanoic acid can be hydrogenated to 1-hexanol (HexOH), an industrially attractive 54 chemical, mainly used within the formulation of synthetic perfumes and detergents, but 55 also as solvent, plasticizer and, more recently, in diesel and gasoline blends [6,7]. Cata-56 lytic hydrogenation of carboxylic acids with molecular H₂ is industrially attractive [8,9], 57 but difficult to achieve, because of the weak polarizability of their C=O group, thus 58 showing a lower reactivity than ketones and aldehydes [10]. In addition, some 59 side-reactions could take place, such as i) decarboxylation of carboxylic acid to alkane, ii) 60 hydrogenolysis of the produced alcohol to alkane, *iii*) esterification between the carbox-61 ylic acid and the produced alcohol [11], summarized in Scheme 1: 62 63



Scheme 1. Possible reactions involved within hexanoic acid hydrogenation.

In the above scheme, in addition to HexOH, also hexyl hexanoate (HexHex) has 66 been highlighted, because of its industrial importance, up to now mainly for fragrances 67 and lubricants production [12]. Remarkably, HexHex has been recently suggested by the 68 United States Department of Energy as a potential blendstock candidate for use in diesel 69 engines [13,14]. Based on the involved reactions (Scheme 1), the hydrogenation should 70 require an active and robust metal and rhenium can represent an interesting alternative 71 to the most expensive noble metals (e.g. Pt, Pd and Ru) [15-17]. Rhenium has several 72 stable oxidation states (e.g. +3, +4, +6, +7) and a reduction step is highly required to obtain 73 the hydrogenating forms, which predominantly include a mixture of +3 and +4 oxidation 74 states, whilst its complete reduction is not feasible without harsh conditions [15, 18–20]. 75 Therefore, rhenium heptoxide (Re₂O₇) reduced in situ by H_2 in a suitable solvent, has 76 been proposed by far as the active catalyst for the hydrogenation of carboxylic acids 77 [15,16]. Many studies involving bimetallic rhenium-based systems are available in the 78 literature, the most relevant related to the hydrogenation of hexanoic acid being sum-79 marized in Table 1, where are compared with the best performances obtained in this 80 work and discussed in the Results. 81

The use of bimetallic systems is proposed to lower the reduction temperature of rhenium, exploiting the strong and close interaction between the two metals, thus improving the selectivity to alcohol_[24–26]. Notwithstanding this, even with bimetallic noble metal/rhenium systems, which are expensive and not commercially available, the carboxylic acid hydrogenation remains difficult to perform, requiring harsh conditions, mainly in term of H₂ pressure, reaction temperature and/or time (Table 1).

From an applicative perspective, commercial rhenium monometallic systems should be preferred over bimetallic ones, being easily available and much less expensive. Their catalytic activity can be increased by performing an appropriate pre-reduction, addressing the selectivity towards the hydrogenation products (e.g. the corresponding alcohol or 91

a mixture of alcohol and its ester) with lower formation of the unwanted alkanes (Scheme 92 1) [19,27]. 93

Table 1. Overview of main relevant data on the hydrogenation of hexanoic acid to HexOH with94rhenium catalysts.95

Hexanoic acid	Catalwat	Т	Р	t	Conversion HexOH yield		Ref.
(g/L)	Catalyst	(°C)	(bar)	(h)	(mol%)	(mol%)	
n.a.	Re ₂ O ₇	200	188	2	n.a.	93	16
46.4	Re-Pt/TiO ₂	130	50	5	58	53	21
23.2	Re-Pd/C	130	20	18	n.a.	74	22
52.6	ReOx-Pd/SiO ₂	140	80	24	100	99	11
14.6	Re-Ni/TiO ₂	180	50	8	100	60	23
93	Re ₂ O ₇	220	115	1	100	70	This work
93	Re/C	220	115	3	100	62	This work

The choice of a commercial catalyst is strategic for developing industrial applications, especially those aimed at exploiting cheap crude carboxylic acid-based substrates 98 working at high concentration and with a substrate as obtained from agro-industrial 99 by-product fermentation adopting simple downstream processing. Raw starting substrates have been scarcely studied for hydrogenation reactions but a preliminary result 101 on the hydrogenation of hexanoic acid ca. 90% pure obtained from red grape pomace 102 fermentation recently suggested the viability of the proposed approach [5]. 103

Now commercial Re₂O₇ and Re/C have been adopted as catalysts for studying the 104 hydrogenation of commercial hexanoic acid. The effect of the wet pre-reduction of rhe-105 nium was investigated, adopting milder reaction conditions respect to dry pre-reduction 106 [28]. Moreover, the effect of the acidity, introduced adopting physical mixtures of the 107 rhenium catalyst with an acid co-catalyst, e.g.as [5 wt% Re/C + niobium phosphate 108 (NbPO)], was also applied for tuning the composition of the alcohol/ester mixture. Af-109 terwards, the optimal identified reaction conditions were applied to the hydrogenation of 110 crude hexanoic acid-rich liquor obtained from white grape pomace anaerobic fermenta-111 tion, containing impurities as other carboxylic acids and water. The nature of this sub-112 strate has determined the choice of using commercial and monometallic rhenium cata-113 lysts rather than ad-hoc prepared and more expensive bimetallic systems. Moreover, the 114 obtained mixture HexOH/HexHex has been evaluated for the first time as potential re-115 newable diesel blendstock. The potential of HexOH as additive to automotive diesel fuel 116 has already been highlighted in many other scientific publications [29,30], while much 117 less interest has been devoted up to now to the adoption of HexHex as blendstock for 118 diesel [31]. The present work shows for the first time the experimental results obtained 119 fueling a Diesel engine with mixtures of Diesel fuel/HexOH/HexHex, with the perspec-120 tive of partially replacing traditional fossil fuels, without modifying the engine perfor-121 mance and achieving significant benefits in reducing soot and CO emissions. 122

2. Results

2.1. Hydrogenation of pure hexanoic acid	12
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2.1.1. Hydrogenation with Re₂O₇

Re₂O₇ was initially tested as the hydrogenation catalyst of commercial hexanoic acid, 126 adopting a lower catalyst loading than that proposed by Broadbent et al. (0.6 wt% vs 0.9 127 wt%, respectively), who reported that the in-situ reduction of Re₂O₇ took place during the 128 reaction [16]. A preliminary study for the identification of the appropriate H₂ pressure to 129 adopt in the hexanoic acid hydrogenation, within a short time scale (within 3-5 hours) 130 was performed._H₂ pressures of 60 and 115 bars have been investigated, working at 210 131 °C, thus preferring milder reaction conditions respect to these of Broadbent et al._[16]. 132

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According to our results (Figure 1), a lower H₂ pressure significantly slows down the reaction rate, advantageously improving the ester yield and limiting the hexane formation, the latter representing the main undesired by-product occurring mainly through the alcohol hydrogenolysis [11].



Figure 1. Influence of H_2 pressure on the pure hexanoic acid hydrogenation in the presence of139Re2O7 at: a) 60 bar; b) 115 bar. Reaction conditions: T = 210 °C; substrate/Re ratio = 270 mol/mol.140

Instead, to direct the reaction towards the preferential formation of HexOH, it is 141 necessary to speed up the hexanoic acid conversion, thus preferably employing a higher 142 H₂ pressure (115 bar). For the same purpose, the temperature was progressively enhanced from 180 to 220 °C, using the same catalyst loading (0.6 wt%, e.g. substrate/Re ratio = 270 mol/mol) and the H₂ pressure of 115 bar (Figure 2). 145



Figure 2. Effect_of temperature on commercial hexanoic acid hydrogenation in the presence of 148 Re₂O₇. Reaction conditions: P H₂ = 115 bar; substrate/Re ratio = 270 mol/mol. 149

The above data highlight the relevant improvement of the hexanoic acid conversion 150 within the shorter reaction times at higher temperatures. Working at 220 °C, an almost 151 complete substrate conversion was reached already after 1 hour of reaction, achieving the 152 maximum HexOH and HexHex yields of about 70 and 20 mol%, respectively (Figure 2). 153 On the other hand, at temperature higher than 210 °C and longer reaction times (Figure 154 2), the HexHex yield remains almost stable, whilst that in HexOH significantly decreases, 155 leading to the undesired hexane formation. These results highlight the possibility of 156 properly tuning the reaction conditions to address the selectivity towards an alco-157 hol/ester mixture. This interesting result prompted us to perform an in-depth investiga-158 tion of the hexanoic acid hydrogenation with the supported commercial system 5 wt% 159 Re/C with the aim of enhancing the catalytic activity respect to Re₂O₇, avoiding metal 160 sintering, and making much easier catalyst recovery and recycle. 161

2.1.2. Hydrogenation with 5 wt% Re/C

Starting from the above results with Re2O7, the monometallic 5 wt% Re/C was em-164 ployed for further investigating the hexanoic acid hydrogenation. At the beginning, 5 165 wt% Re/C was characterized through ICP-OES, N2 physisorption, TEM and H2-TPR 166 techniques, finding that this catalyst has 4.8 wt% of rhenium content, 840 m²/g of specific 167 surface area, and 1.68 nm of rhenium average particle size, according to Figure 3.

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Figure 3. TEM picture of 5 wt% Re/C and the respective distribution of the Re particle sizes and the 171 Gaussian fitting. 172

Moreover, a maximum peak H₂-TPR temperature at 400 °C was found (Figure 4), 173 attributed to the complete reduction of the metal which is present in the sample with the 174 highest oxidation state 7+ [32], this temperature being higher than those generally reported for other noble metals, confirming that Re is hardly reducible to 0 state [28,33]. 176



As received 5 wt% Re/C was preliminarily tested under the best reaction conditions, 182 identified for the Re₂O₇ catalyst (T = 220 °C, P H₂ = 115 bar; substrate/Re ratio = 270 183 mol/mol), and a maximum hexanoic acid conversion of about 90 mol% was reached after 184 3 hours (Figure 5a). 185

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The reaction proceeds more slowly than that with Re₂O₇ (Figure 2), and an almost 190 equimolar mixture of HexOH/HexHex was obtained after 3 hours, due to the lower ac-191 tivity of 5 wt% Re/C, indicative of a more difficult in-situ reducibility of 5 wt% Re/C. Lit-192 erature reports that rhenium is active for hydrogenation reactions as a mixture of oxi-193 dized species, but generally a pre-reduction step allows to reduce the average oxidation 194 state of the Re species, mainly up to the active states 3+ and 4+ [15]. Therefore, a wet 195 pre-reduction was adopted for improving the activity of the 5 wt% Re/C, adopting a 196 much milder temperature (180 °C), e.g. more sustainable conditions, if compared with 197 the traditional dry method (at least 400 °C) [34]. This choice is further supported by the 198 well-known difficulty in obtaining the completely reduced rhenium, even under partic-199 ularly severe conditions [18]. XPS spectroscopy was used to evaluate the oxidation state 200 of rhenium within the as received and pre-reduced catalyst under our wet conditions, 201 thus demonstrating the effectiveness of the proposed approach (Figure 6). XPS spectrum 202 of the as received 5 wt% Re/C reveals the sole presence of Re^{7+} , with the 4d7/2 component 203 centered at about 45.9 eV, in agreement with the results of Rozmysłowicz et al. [20]. After 204 the pre-reduction, XPS analysis (Figure 6) still shows the presence of Re^{7+} , but in lower 205 amount (43%), because additional bands are found at 41.4 and 43.1 eV, which are char-206 acteristic of Re³⁺ (30 %) and Re⁴⁺ (27%) species, respectively [32,35]. 207



Figure 6. XPS spectra of fresh and pre-reduced commercial 5 wt% Re/C.

The effectiveness of this mild pre-reduction on the catalytic performances was evi-212 denced by the comparison of the performances between the hydrogenation carried out 213 with the as received and pre-reduced 5 wt% Re/C, adopting the same reaction conditions 214 (Figure 5). In fact, the complete conversion of the hexanoic acid was achieved after 3 215 hours, with maximum HexOH and HexHex yields of 62 mol% and 31 mol%, respectively, 216 when the pre-reduced 5 wt% Re/C catalyst was employed. Also the spent catalyst was 217 characterized by XPS analysis, confirming the presence of Re³⁺_(41%) and Re⁴⁺_(59%) spe-218 cies (Figure 7), thus proving that the reduction of all the Re^{7+} species occurs during sub-219 strate hydrogenation, this improving the catalytic activity of 5 wt% Re/C system. 220



Figure 7. XPS spectra of spent commercial 5 wt% Re/C.

2.1.3. Hydrogenation in the presence of NbPO as the acid co-catalyst

The possibility of shifting the selectivity towards HexHex formation was evaluated 225 by adopting commercial NbPO as the acid co-catalyst. This protonic solid is characterized 226 by Lewis acidity assigned to unsaturated Nb⁵⁺ sites, while Brønsted acidity is mainly 227 originated by P-OH groups and, in lesser extent, by Nb-OH sites [36]. The water-tolerant 228 NbPO is characterized by a specific surface area of 133 m²/g and a total acidity of 0.33 229 mmol/g,_with a predominant fraction of low-medium strength sites and a relatively 230 smaller fraction of stronger sites [37,38]. Several physical mixtures of pre-reduced 5 wt% 231 Re/C with different amounts of NbPO have been tested for hexanoic acid hydrogenation, 232 aimed at maximizing the ester formation, thus simplifying the screening of the appro-233 priate (acid) catalyst dosage. The hydrogenation of hexanoic acid with 5 wt% Re/C + 234 NbPO was carried out under the same conditions already adopted for pre-reduced 5 wt% 235 Re/C system (220 °C, 115 bar, 3 h) and the corresponding data are reported in Figure 8. 236

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Figure 8. Effect of the acidity of the proposed acidic catalytic systems towards the hydrogenation of238commercial hexanoic acid. Reaction conditions: T = 220 °C; $P H_2 = 115$ bar; t = 3 h; substrate/Re ratio239of 270 mol/mol.240

The results confirm that the presence of acidity markedly favors the ester formation. 241 A moderate slowdown of the hexanoic acid conversion was ascertained by increasing the 242 NbPO amount, probably due to lower stirring efficiency and diffusion limitations in the 243 slurry, but a much more relevant improvement of the HexHex selectivity was obtained. 244 In particular, the physical mixture composed of 5 wt% Re/C + 2 g of NbPO led to the 245 highest HexHex selectivity of about 70 mol% (corresponding to a yield of about 60 246 mol%), keeping low the hexane selectivity (<15 mol%). On the other hand, the increase of 247 NbPO amount up to 3 g did not further improve the ester selectivity, rather enabling the 248 hexane formation and making stirring difficult. Therefore, the proper acidity of the cat-249 alytic system plays a key role to address the selectivity of the reaction towards esterifica-250 tion, favoring the preferential production of HexHex. 251

2.2. Hydrogenation of crude hexanoic acid

The hydrogenation was then performed on a real crude hexanoic acid, obtained 254 through the anaerobic fermentation of the white grape pomace. In our preliminary study 255 [5], the first results on hydrogenation of hexanoic acid from fermented red grape pomace 256 with 5 wt% Re/C, were showed. However, wine making process also produces white 257 grape pomace which, differently from the red one, does not undergo alcoholic fermenta-258 tion, thus resulting poorer in ethanol and richer in fermentable sugars [39]. The compo-259 sitional differences of the biomasses might have relevant repercussions on the chemical 260 composition of the corresponding fermented liquors and the proposed cascade process 261 should be robust, i.e. poorly dependent on compositional variations of the fermented 262 crude liquor. Anaerobic fermentation of white grape pomace was carried out under the 263 previously reported reaction conditions [5]. Hexanoic acid purity was determined by 264 GC-FID technique and resulted appreciably higher than that of the corresponding liquor 265 deriving from red grape pomace fermentation (93 vs 87 wt% for white and red grape 266 pomace, respectively). GC-MS analysis of the crude fermented white grape pomace al-267 lowed to identify, in addition to hexanoic acid as the main target compound, only few 268 carboxylic acids in the range C4-C8 as the minor compounds (Figure S1 and Table S1). 269 Hydrogenation of the crude fermented white grape pomace was carried out with the 270 most performing Re-based catalysts, addressed to the more selective production of 271

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HexOH (5 wt% Re/C) and of HexHex (physical mixture of 5 wt% Re/C+ 2 g of NbPO), 272 adopting the best identified reaction. The obtained results are reported in Figure 9: 273

Figure 9. Hydrogenation of crude hexanoic acid from white grape pomace with (a) 5 wt% Re/C and 276 b) physical mixture [5 wt% Re/C + 2 g NbPO]. Reaction conditions: T = 220 °C; P H₂ = 115 bar; sub-277 strate/Re ratio of 270 mol/mol. 278

Remarkably, when crude hexanoic acid obtained from fermentation of white grape 279 pomace was employed as the substrate, the conversion was only slightly lower than that 280 ascertained for the pure hexanoic acid. The selectivity behaviors towards HexOH and 281 HexHex agree with those achieved in the hydrogenation of commercial hexanoic acid 282 (compare Figure 9 with Figure 5 and Figure 8), thus proving the tunability and the ro-283 bustness of the adopted catalytic systems. In both cases, hexane formation was kept low, 284 highlighting the successful optimization of the reaction conditions. The reaction mixture 285 deriving from white grape pomace hydrogenation shows the presence of HexOH, butyl 286 butanoate, HexHex and hexyl octanoate (Figure S2 and Table S2). The chemical stability 287 of both employed catalytic systems was demonstrated up to five recycling tests (Figure 288 10), a relevant characteristic for the successive scale-up of this process. In fact, it was 289 possible to observe only a slight decrease of the hexanoic acid conversion with the pro-290 gress of the recycling tests, mainly due to the partial loss of the catalytic systems during 291 the filtration, recovery and recycling steps, rather than due to rhenium leaching from the 292 catalysts. 293



Figure 10. Recyclability tests of: a) 5 wt% Re/C; b) physical mixture [5 wt% Re/C + 2 g NbPO] employed in the hydrogenation of crude hexanoic acid from white grape pomace. Reaction conditions: T = 220 °C; P H₂ = 115 bar; t = 3 h; substrate/Re ratio of 270 mol/mol.

This was confirmed by the ICP analysis showing that the Re content in the reaction 301 mixtures recovered at the end of the fifth recycle was below the detection limit, indicating 302 that leaching of Re was negligible for both catalytic systems (5 wt% Re/C and the physical 303 mixture 5 wt% Re/C and NbPO). The absence of rhenium leaching has been further con-304 firmed by removal of bulk 5 wt% Re/C from the reaction mixture recovered after 3 h of 305 hydrogenation of crude hexanoic acid from white grape pomace (Figure 9a). The addi-306 tion of fresh hexanoic acid to the recovered reaction mixture and the continuation of the 307 reaction for other 3 h have confirmed the absence of further hydrogenation products. 308

2.3. Engine tests results

A mixture of 5.2 vol% of HexOH + 4.8 vol% of HexHex, corresponding to a molar 311 ratio of about 2/1 mol/mol, was selected as a model of the reaction mixture obtained in 312 the hydrogenation performed in the presence of pre-reduced Re/C (Figure 5b). This 313 mixture (10 vol%) was added to 90vol% of Diesel fuel,_without any phase separation. The 314 resulting blend has been tested in the experimental engine and compared with Diesel fuel 315 alone and with the two mixtures of the single components with Diesel, i.e. 10 vol% of 316 HexOH with 90% Diesel fuel [10HexOH] and 10% HexHex with 90 vol% Diesel fuel 317 [10HexHex]. These last two mixtures have been employed as reference to better under-318 stand the influence of the single components, alcohol and ester, on engine performance 319 adopting the same conditions. 320

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The main physicochemical properties of the used fuels are reported in Table 2.

	Diesel	HexOH	HexHex
Density (g/cm ³)	0.837	0.815	0.863
Cinematic Viscosity (at 40 °C – cst)	≈ 2.7	3.64	2.37
Flash Point (°C)	55	63	102
Cetane Number (CN)	> 50	23	40
Boiling Point (°C)	180–360	157	205
Lower Heating Value (MJ/Kg)	≈ 43	39	35

Table 2. Main characteristics of the utilized fuels.

The mixtures previously described have been utilized at maximum loads and dif-324 ferent rpm, i.e.at 1500, 2000 and 2500 rpm, whilst injection timing was maintained fixed 325 along the experimentation. As reported in Figure 11a, the use of different blending with 326 Diesel does not significantly affect the power-rpm curve of the employed engine. The 327 HexOH/HexHex mixtures employed for the tests resulted only in a slightly lower power: 328 since the fuel volumetric flow is constant, due to the volumetric injection system, the 329 lower power can be explained by the reduced LHV of the employed mixtures with re-330 spect to the Diesel fuel. Remarkably, the use of the HexOH/HexHex mixtures led to a 331 decrease in the CO emissions, as reported in Figure 11b, mainly owing to the higher H/C 332 ratio in the fuel molecule (compared to Diesel), and to the presence of oxygen, which 333 enhances the carbon complete oxidation during combustion [40]. As evidenced in Figure 334 11c, HC emissions result higher when Diesel combustion is realized within the 335 co-presence of HexHex, rather than HexOH. This behavior is apparently in contrast with 336 the higher cetane number of HexHex (if compared with that of HexOH), whilst a de-337 crease in HC formation should be expected (given by the shorter combustion delay, re-338 sulting in enough time for realizing HC oxidation). In our case, the ascertained delay 339 combustion (higher HC formation), caused by the HexHex, could be due to its 340 self-ignition properties, mainly defined by its higher boiling point and flash point tem-341 perature. On the other hand, the lower cetane number of HexOH and HexHex (respect to 342 that of Diesel) only slightly enhances NOx emissions (Figure 11d), thus indicating that the 343 maximum combustion temperature moderately increases in the case of the die-344 sel-HexHex/HexOH blendstocks. Here, the ignition delay increases the amount of fuel 345 required within the first part of the combustion process and, consequently, the release 346 rate of the combustion heat. Lastly, a significative reduction of the soot emissions was 347 ascertained in the case of the diesel-HexOH-HexHex blendstocks (Figure 11e), achieving 348 a reduction of about 50% at higher rpm. This noteworthy result is due to the lower carbon 349 content (lower C/H ratio) of the employed mixtures, which reduces the carbon availabil-350 ity for soot formation, and the oxygen promotes the oxidation processes. Moreover, the 351 lower boiling points of the oxygenated compounds lead to a kind of "droplet explosion" 352 once the fuel mixture is introduced in a hot environment [41,42], improving fuel atomi-353 zation and mixing, thus leading to the combustion completion of the carbon-based mol-354 ecules. 355 356

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Figure 11. Engine performances, in term of a) engine power; b) CO emission; c) HC emission; d) NO_x emission and e) soot emission, all evaluated at the maximum load.

3. Materials and Methods

3.1. Materials

Hexanoic acid (>99%), n-dodecane (>99%), hexane (>99%), hexyl hexanoate (>98%), 1-hexanol (>99%), methanol (>99%), n-octane (99%) and Re₂O₇ were purchased by Sigma-Aldrich. 5 wt% Re/C was provided by Riogen, whilst NbPO by CBMM (Compahia Brasileira de Metalurgia e Mineracão) and used after treatment at 255 °C for 6 h under high vacuum.

Grape pomace, deriving from white wine production, was kindly provided by 367 Caviro Distillerie (Faenza, Italy), and used without any pre-treatment. Crude hexanoic 368 acid-rich liquor was produced from white grape pomace according to the previously 369 reported procedure slightly modified. Briefly, the white grape pomace was fed into a 370 leaching process with water which allowed to obtain: 1) the ethanol solution (30 g/L) to 371 be fermented for hexanoic acid production; and 2) the grape pomace that could be further 372 valorized through conventional process (tartaric acid, seed oil extraction; out of the focus 373 of this work). Thereafter, the ethanol solution was fermented and hexanoic acid was ex-374 tracted as previously reported [5]. The obtained crude hexanoic acid was later charac-375 terized. 376

3.2. Catalyst characterization

Temperature programmed reduction by H₂ (H₂-TPR) was performed in an AutoChem II apparatus (Micromeritics). The catalyst was firstly treated at 300 °C under He flow of 50 mL/min for 30 min for the removal of impurities. After cooling to 50 °C, the carrier gas was switched to 5 vol% H₂/Ar, with a flow of 40 mL/min. When the baseline was stable, the temperature was increased up to 800 °C, with a heating rate of 10 °C/min. The amount of consumed H₂ was measured with a thermal conductivity detector (TCD). 384

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X-ray photoelectron spectroscopy (XPS) measurements were conducted with a VSW 385 TA10 twin anode, adopting the X-ray AlK α source (emission: 10 mA, voltage 10 kV), and 386 a hemispherical electron energy analyzer VSW HA100. 387

A single point ThermoQuest Surface Area Analyzer Qsurf S1 was used for Specific Surface Area (SSA) analysis of the supported rhenium catalysts, according to the experimental procedure reported in our previous work [43].

Transmission Electron Microscopy (TEM) measurements in bright field mode were conducted with a CM12 microscope (Philips), operating at 120 keV, as previously reported [44].

The rhenium content both in the as-received catalyst and in the liquid sample col-394 lected at the end of the recycle runs was determined by inductively coupled plas-395 ma-optical emission spectrometry (ICP-OES), using an Optima 7000 DV (PerkinElmer) 396 analyser equipped with a CCD array detector and the emission line of 221.43 nm was 397 adopted. 398

3.3. Hydrogenation procedure

Hydrogenation reactions were carried out in a 300 mL stainless steel Parr 4560 autoclave 401 equipped with a P.I.D. controller (4848). 5 wt % Re/C was pre-reduced in methanol (180 402 °C, 90 bar of H₂, 6 h) as previously reported [5], whilst Re₂O₇ was directly employed 403 without any pre-reduction step. The reaction mixture was stirred using a mechanical 404 overhead stirrer. The reactor was pressurized with hydrogen up to the selected value 405 determined at a reaction temperature, pressure being held constant by automatically 406 feeding more hydrogen. At the end of the reaction, the reactor was rapidly cooled at 407 room temperature, depressurized and the reaction mixture was filtered to remove the 408 catalyst and finally analysed through GC/FID and GC/MS chromatography. For the 409 recycling tests, the spent catalyst was recovered by filtration under argon atmosphere, 410properly washed, and recycled following to the same procedure as adopted for the direct 411 run. 412

3.4. Product analysis

The liquid samples were analyzed using GC-FID (DANI GC1000) equipped with a 415 HP-PONA column (20 m \times 0.2 mm \times 0.5 μ m). N₂ was employed as the carrier gas with the 416 flow rate of 1 mL/min. Both injector and detector were kept at 250 °C and the following temperature program was employed for the chromatographic runs: 150 °C for 5 min; 12 418 °C/min up to 200 °C; 200 °C for 2 min; 15 °C/min up to 250 °C; 250 °C for 10 min. The 419 moles of analytes were calculated from_the calibration with standard solutions. The 420 analyses were carried out in triplicate and the reproducibility of the technique was within 421 the 5%. 422

The identification of the compounds of interest was performed by GC-MS (Agilent 423 7890B-5977A), equipped with a HP-5MS column (30 m \times 0.25 mm \times 0.25 μ m). Helium was 424 adopted as carrier gas, with the flow rate of 1 mL/min. Injector and detector were kept at 425 250 and 280 °C, respectively, and the following temperature program was employed for 426 the chromatographic runs: 60 °C for 1 min; 10 °C/min up to 200 °C; 200 °C for 2 min; 5 427 °C/min up to 220 °C; 220 °C for 20 min; 10 °C/min up to 270 °C; 270 °C for 1 min. 428

3.5. Engine experimental setup

A Lombardini-Kohler Diesel engine model 9LD 625/2, whose specifications have 431 been previously reported has been utilised and coupled with a Borghi&Saveri eddy cur-432 rent brake with rpm/Torque controller.30 Emission analysis was performed as previously 433 reported [45]. 434

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4. Conclusions

In this work, the hydrogenation of commercial hexanoic acid has been investigated 438 for the synthesis of 1-hexanol/hexyl hexanoate mixtures, employing different rhenium 439 heterogeneous catalysts. The activity of the reaction was enhanced by a mild 440 pre-reduction step, while the selectivity of the reaction was strongly affected by acidic 441 properties of the overall catalytic systems. In fact, under the same reaction conditions, the 442 selectivity of the 5 wt% Re/C catalyst was mainly addressed towards 1-hexanol, whilst 443 the employment of rhenium-based acid catalytic system, such as a physical mixture [5 444 wt% Re/C + niobium phosphate], significantly shifted the selectivity towards hexyl hex-445 anoate formation. Catalytic hydrogenation of the crude hexanoic acid, deriving from 446 acidogenic fermentation of white grape pomace without any purification, with 5 wt% 447 Re/C and with the physical mixture [5 wt% Re/C + niobium phosphate] gave similar re-448 sults to those achieved with the commercial hexanoic acid, even after up to five recycle 449 runs, thus highlighting the robustness of the process, the proper choice of the catalyst 450 resulting strategic to modulate the composition of the final mixture. Engine tests confirm 451 the potentiality of these mixtures as novel diesel bio_blendstocks, able to reduce the 452 emissions of particulate and CO without any significant increasing of NOx emission or 453 changing in engine performance, thus contributing to meet the greenhouse gases emis-454 sion reductions target and to the partial replacement of traditional fossil fuels, in ac-455 cordance with the short-term goals of the EU countries. 456

Supplementary Materials: The following supporting information can be downloaded at: 458 www.mdpi.com/xxx/s1, Figure S1: Total ion chromatogram (TIC) of crude fermented white grape 459 pomace; Figure S2: Total ion chromatogram (TIC) of post-hydrogenated white grape pomace; Table 460 S1: Products identified in the crude fermented white grape pomace; Table S2: Products identified in 461 the crude fermented white grape pomace. 462

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